

# **Ultrafast Optical Physics II (SoSe 2021)**

## **Lecture 21, June 17**

- 1) Ultrashort Pulse Optical Parametric Amplification**
- 2) Non-collinear Optical Parametric Amplification**
- 3) Optical Parametric Chirped Pulse Amplifier (OPCPA)**
- 4) Optical Synthesis from OPAs**

**[5] Largely follows the review paper of Cerullo et al., “Ultrafast Optical Parametric Amplifiers” Rev. Sci. Instr. 74, pp 1-17 (2003)**

# Ultrashort Pulse Optical Parametric Amplification

$$\vec{E}_{p,s,i}(z, t) = \text{Re} \left\{ E_{p,s,i}(z, t) e^{j(\omega_{p,s,i}t - k_{p,s,i}z)} \vec{e}_{p,s,i} \right\}$$

Pulse envelopes

$$\begin{aligned} \frac{\partial E_p}{\partial z} + \frac{1}{v_p} \frac{\partial E_p}{\partial t} &= -j\kappa_p E_s E_i e^{j\Delta kz} , \\ \frac{\partial E_s}{\partial z} + \frac{1}{v_s} \frac{\partial E_s}{\partial t} &= -j\kappa_s E_p E_i^* e^{-j\Delta kz} , \\ \frac{\partial E_i}{\partial z} + \frac{1}{v_i} \frac{\partial E_i}{\partial t} &= -j\kappa_i E_p E_s^* e^{-j\Delta kz} , \end{aligned}$$

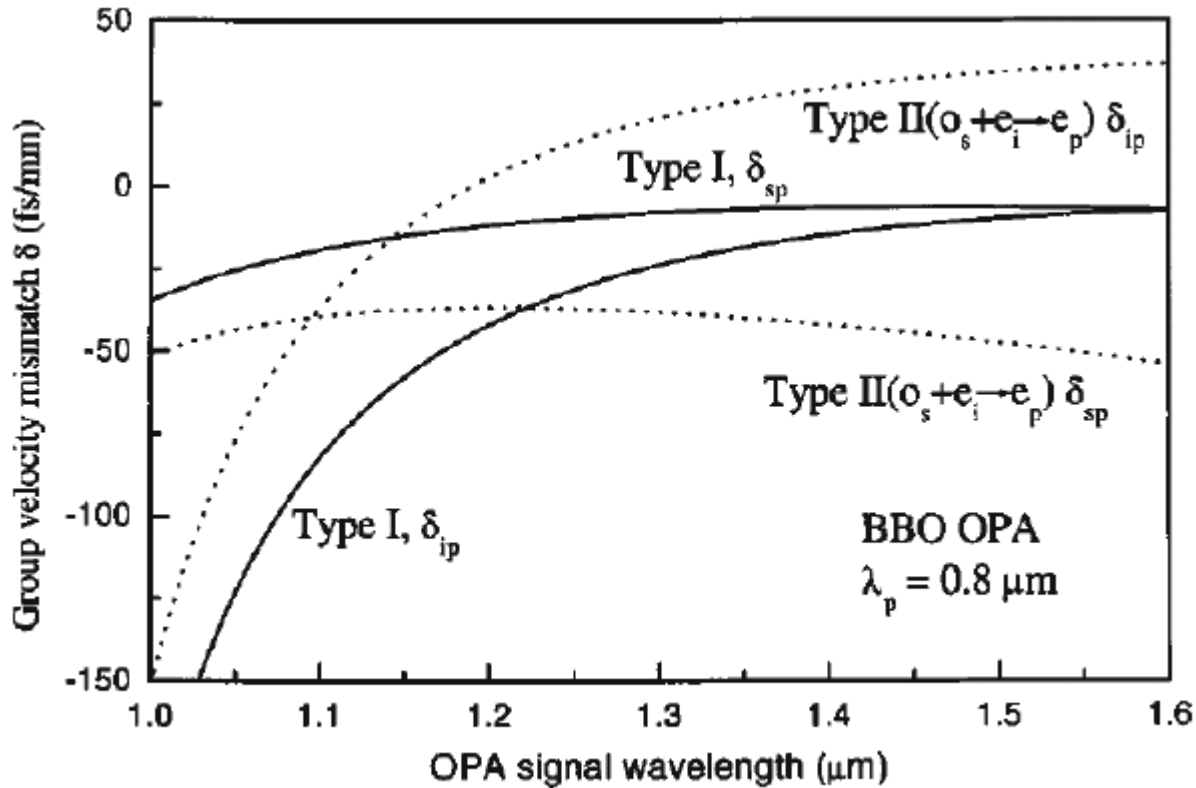
$v_{p,s,i} = dk/d\omega|_{\omega_{p,s,i}}$  are the corresponding group velocities

$$\begin{aligned} t' = t - z/v_p \quad \frac{\partial E_p}{\partial z} &= -j\kappa_p E_s E_i e^{j\Delta kz} , \\ \frac{\partial E_s}{\partial z} + \left( \frac{1}{v_s} - \frac{1}{v_p} \right) \frac{\partial E_s}{\partial t} &= -j\kappa_s E_p E_i^* e^{-j\Delta kz} , \\ \frac{\partial E_i}{\partial z} + \left( \frac{1}{v_i} - \frac{1}{v_p} \right) \frac{\partial E_i}{\partial t} &= -j\kappa_i E_p E_s^* e^{-j\Delta kz} . \end{aligned}$$

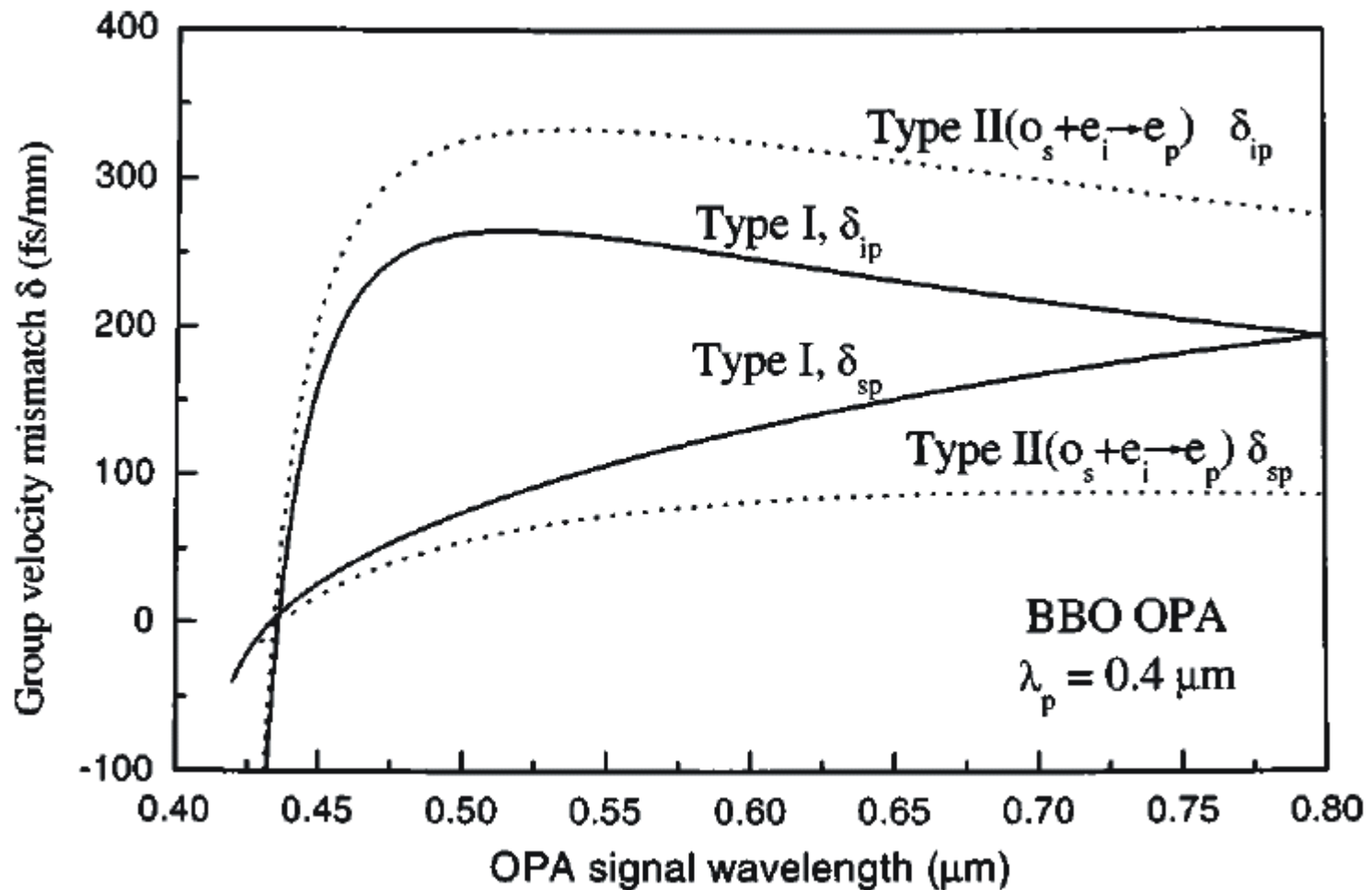
Temporal walkoff  
Group Velocity Mismatch (GVM)

Pump pulse width

$$l_{jp} = \frac{\tau}{\delta_{jp}}, \text{ with } \delta_{jp} = \left( \frac{1}{v_j} - \frac{1}{v_p} \right)$$



**Fig. 12.31:** Pump-signal ( $\delta_{sp}$ ) and pump-idler ( $\delta_{ip}$ ) group velocity mismatch curves for a BBO OPA at the pump wavelength  $\lambda_p = 0.8 \mu\text{m}$  for type I phase matching (solid line) and type II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line).



**Fig. 12.32:** Pump-signal ( $\delta_{sp}$ ) and pump-idler ( $\delta_{ip}$ ) group velocity mismatch curves for a BBO OPA at the pump wavelength  $\lambda_p = 0.4 \mu\text{m}$  for type I phase matching (solid line) and type II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line).

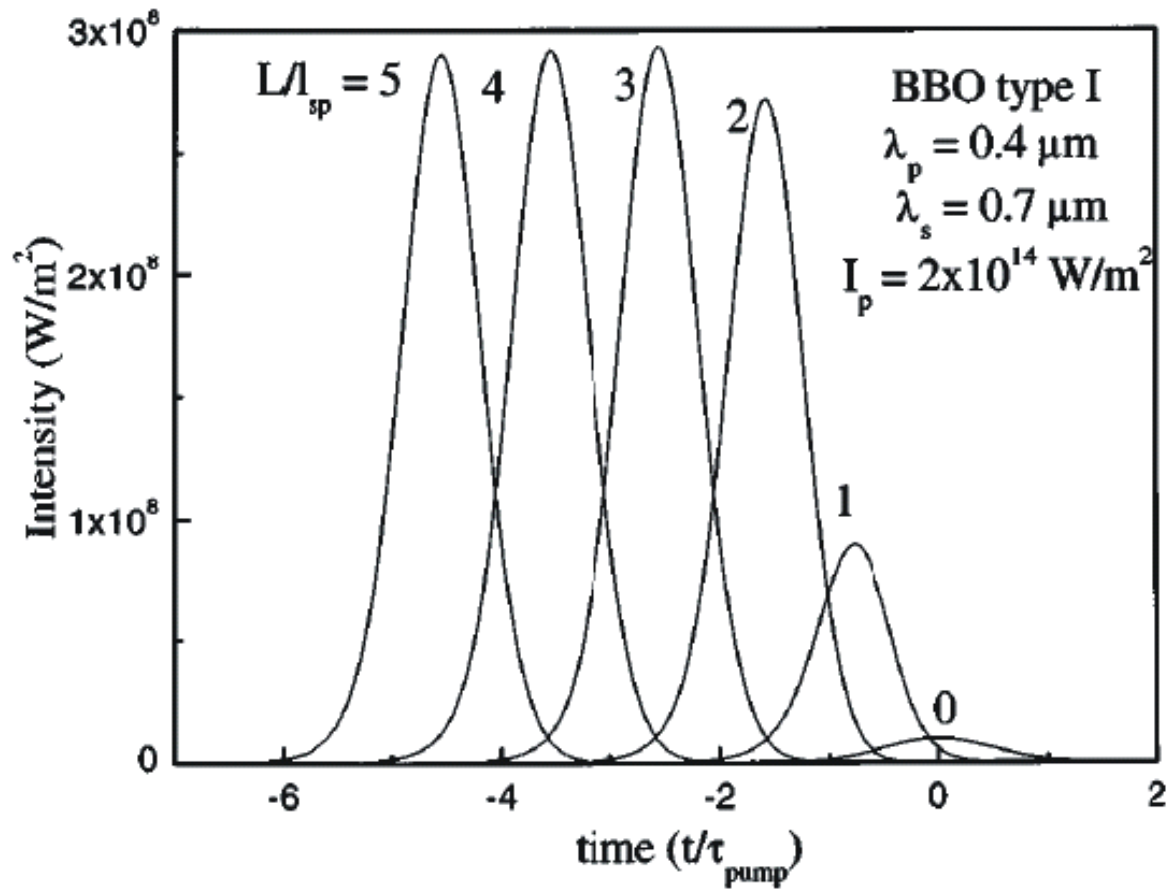


Figure 12.34: Signal pulse evolution for a BBO type I OPA with  $\lambda_p = 0.4 \mu\text{m}$ ,  $\lambda_s = 0.7 \mu\text{m}$ , for different lengths  $L$  of the nonlinear crystal. Pump intensity is  $20 \text{ GW/cm}^2$ . Time is normalized to the pump pulse duration and the crystal length to the pump-signal pulse splitting length. [5]

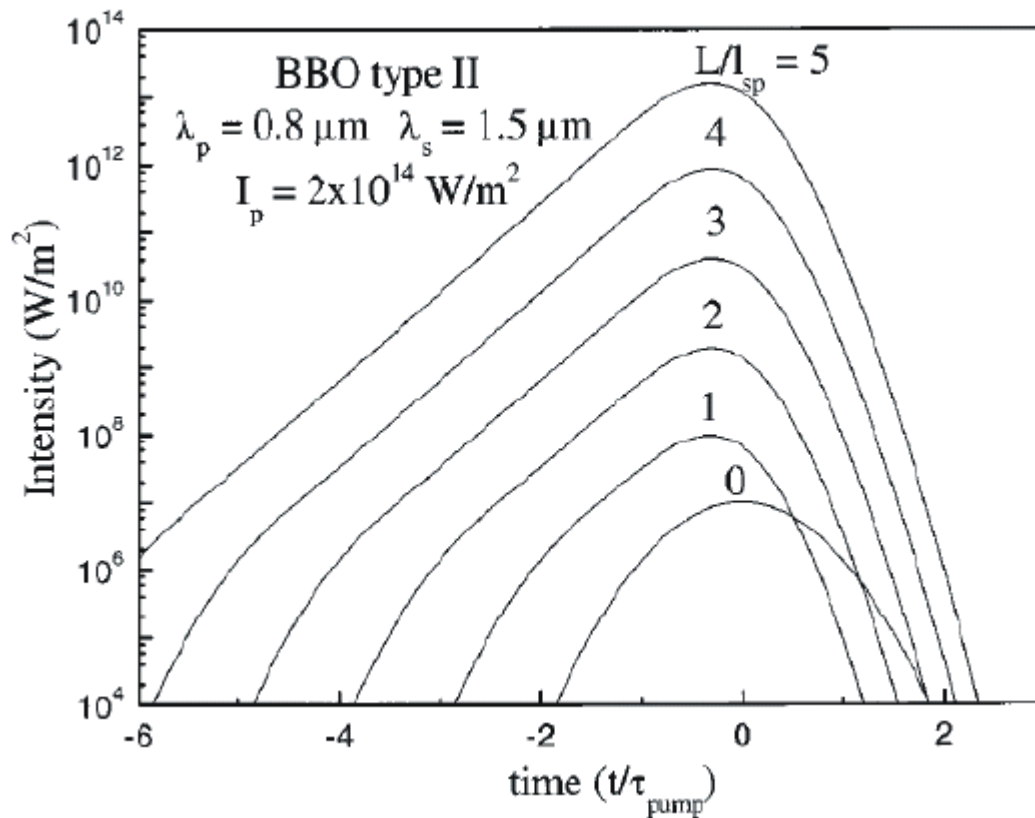


Figure 12.35: Signal pulse evolution for a BBO type II OPA with  $\lambda_p = 0.8 \mu\text{m}$ ,  $\lambda_s = 1.5 \mu\text{m}$ , for different lengths  $L$  of the nonlinear crystal. Pump intensity is  $20 \text{ GW/cm}^2$ . Time is normalized to the pump pulse duration and the crystal length to the pump-signal pulse splitting length. [5]

# OPA Bandwidth

$$\omega_s \longrightarrow \omega_s + \Delta\omega \quad \omega_i \longrightarrow \omega_i - \Delta\omega.$$

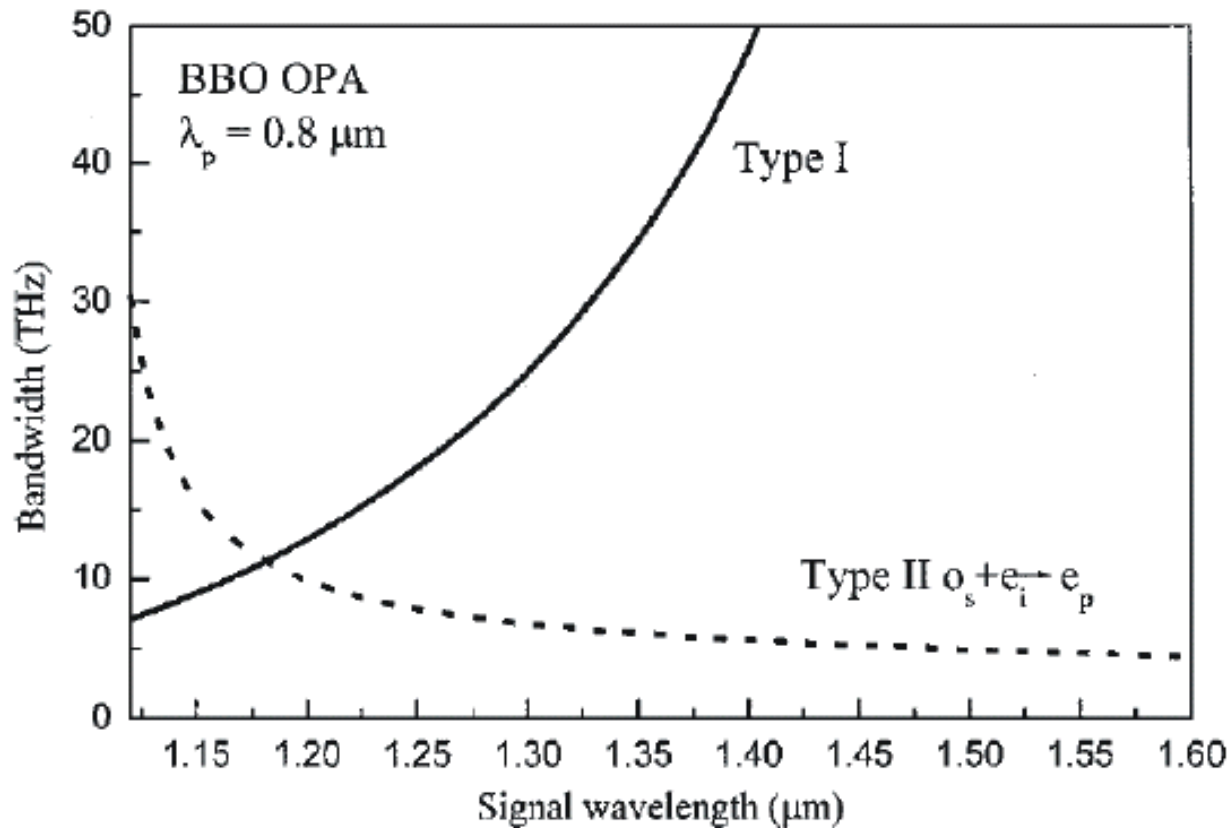
$$\Delta k = -\frac{dk_s}{d\omega} \Delta\omega + \frac{dk_i}{d\omega} \Delta\omega = \left( \frac{1}{v_i} - \frac{1}{v_s} \right) \Delta\omega$$

## Bandwidth limitation due to GVM

$$\Delta f = -\frac{2\sqrt{\ln 2}}{\pi} \sqrt{\frac{\Gamma}{L}} \frac{1}{\left| \frac{1}{v_i} - \frac{1}{v_s} \right|}$$

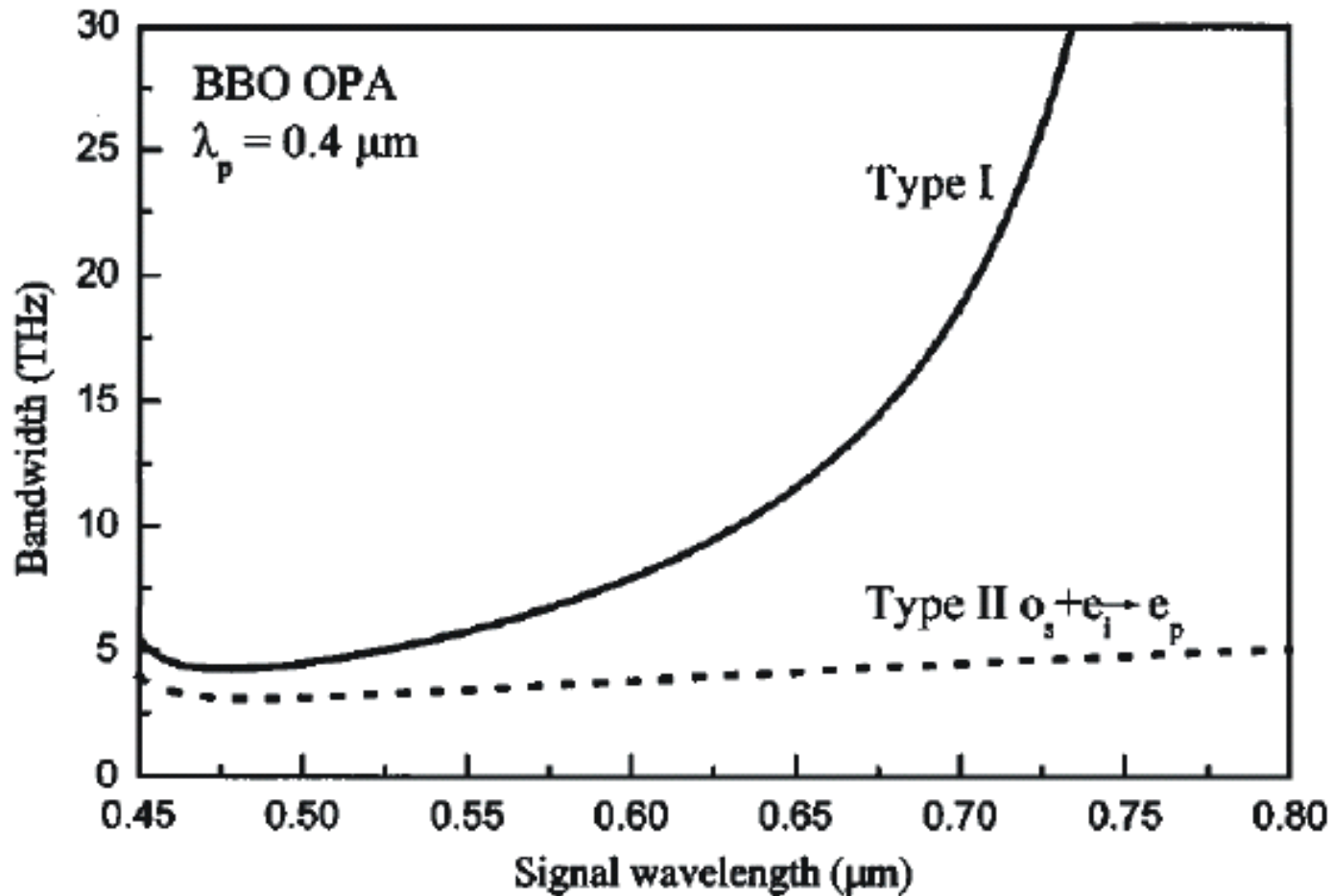
**For vanishing dispersion:**

$$\Delta f = -\frac{2\sqrt[4]{\ln 2}}{\pi} \sqrt[4]{\frac{\Gamma}{L}} \frac{1}{\left| \frac{d^2 k_s}{d\omega^2} + \frac{d^2 k_s}{d\omega^2} \right|}.$$



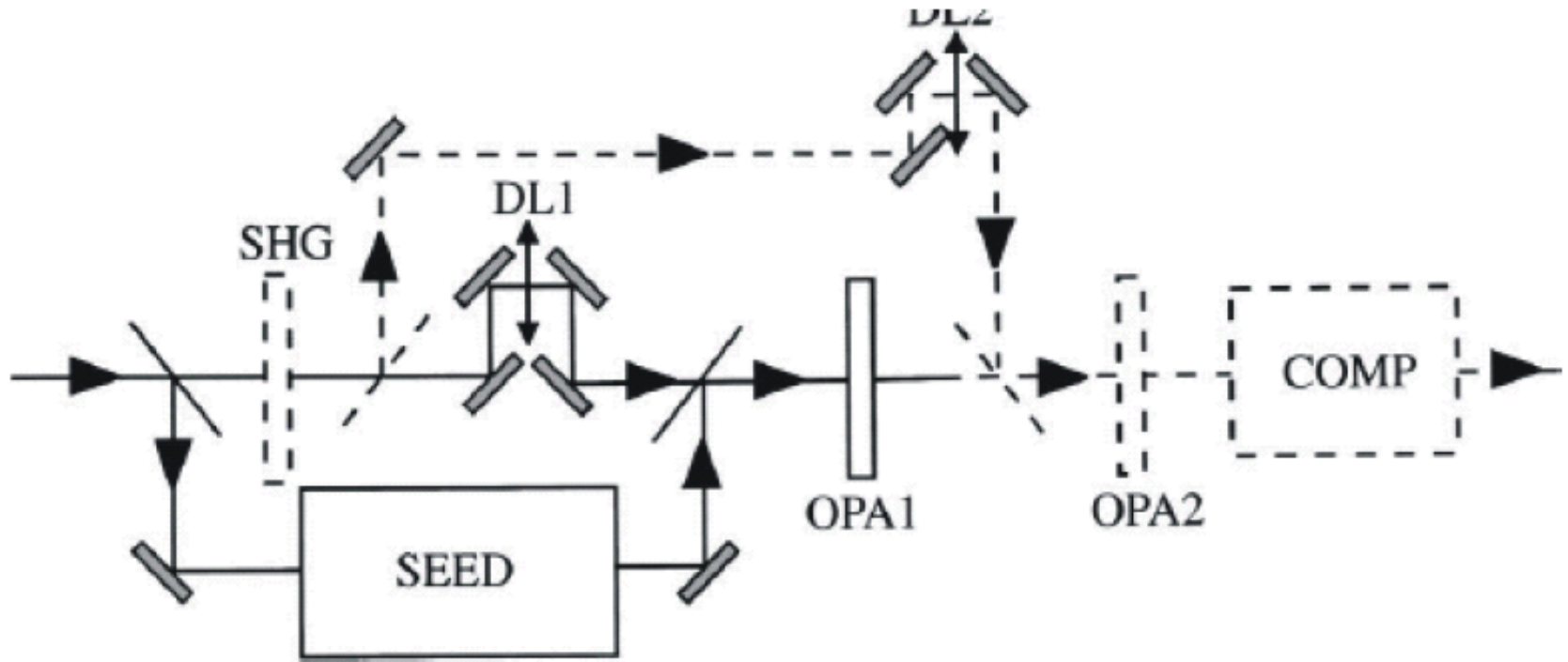
**Figure 12.35:** Phase matching bandwidth for a BBO OPA at the pump wavelength  $\lambda_p=0.8 \mu\text{m}$  for type I phase matching (solid line) and type II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line). Crystal length is 4 mm and pump intensity 50 GW/cm<sup>2</sup>.





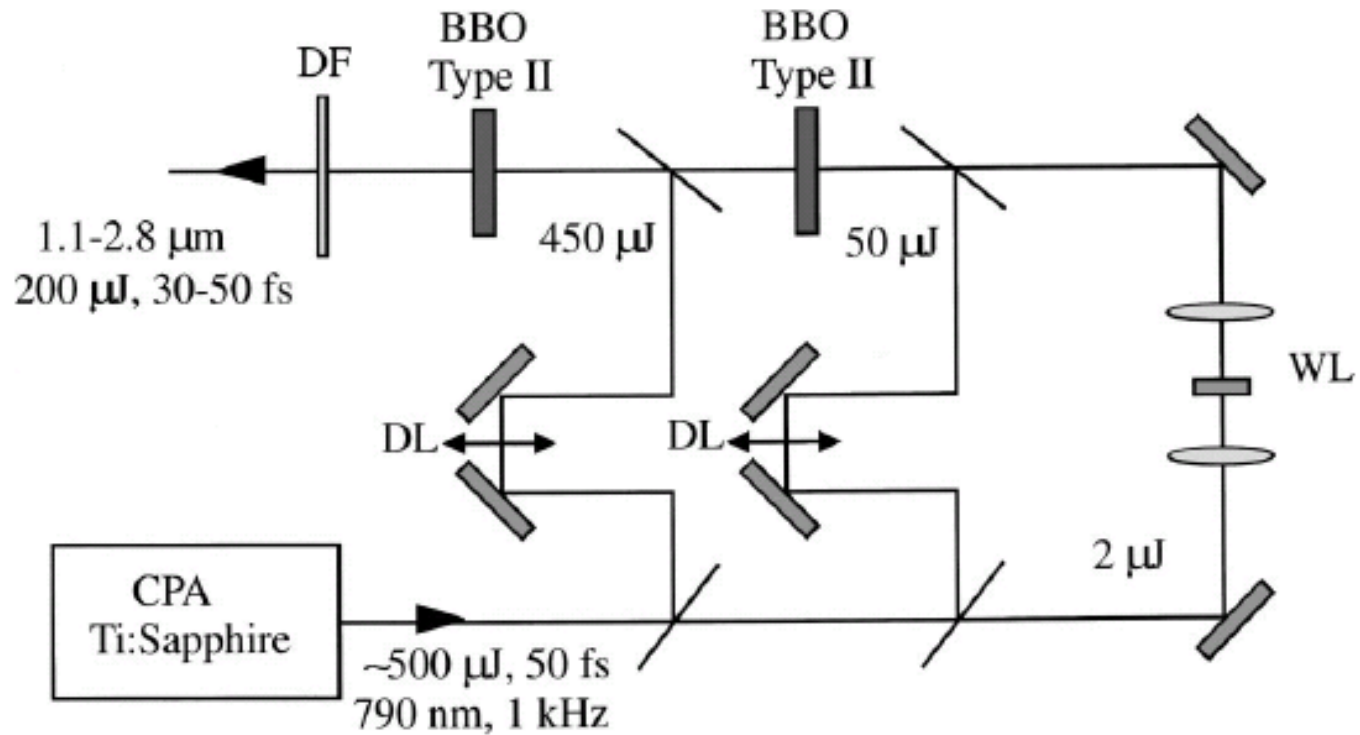
**Figure 12.36:** Phase matching bandwidth for a BBO OPA at the pump wavelength  $\lambda_p=0.4 \mu\text{m}$  for type I phase matching (solid line) and type II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line). Crystal length is 2 mm and pump intensity  $100 \text{ GW/cm}^2$ .

# Optical Parametric Amplifier Designs



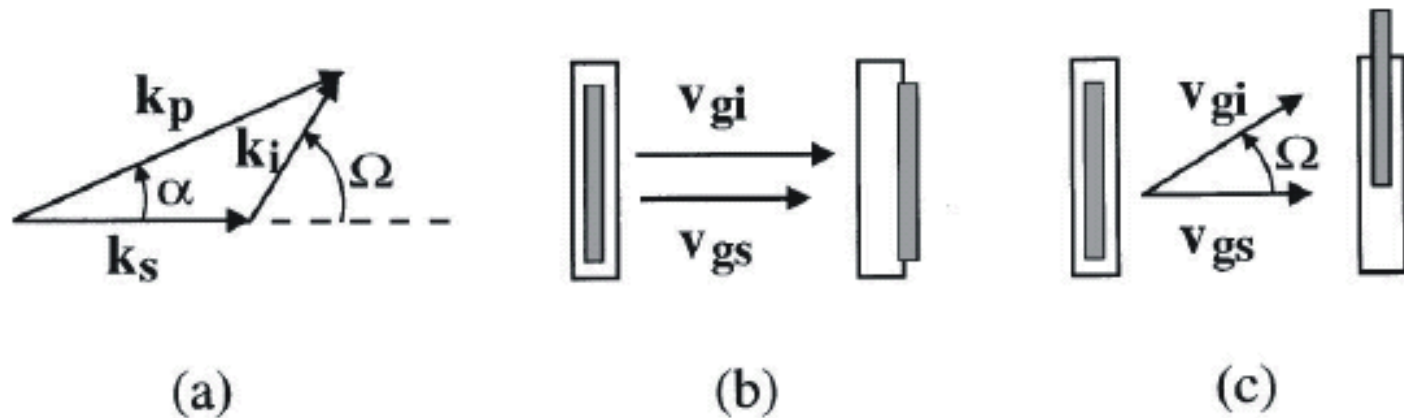
**Figure 12.37:** Scheme of an ultrafast optical parametric amplifier. SEED: seed generation stage; DL1, DL2: delay lines; OPA1, OPA2 parametric amplification stages; COMP: compressor.

# Near-IR OPA



**Figure 12.38:** Scheme of a near-IR OPA DL: delay lines; WL: white light generation stage; DF: dichroic filter. [5]

# Noncollinear Optical Parametric Amplifier (NOPA)



**Figure 12.39:** a) Schematic of a noncollinear interaction geometry; b) representation of signal and idler pulses in the case of collinear interaction; and c) same as b) for noncollinear interaction.

## Phase Matching Condition: Vector Condition:

$$\Delta k_{par} = k_p \cos \alpha - k_s - k_i \cos \Omega = 0$$

$$\Delta k_{perp} = k_p \sin \alpha - k_i \sin \Omega = 0$$

## Variation on phase matching condition by $\Delta\omega$

$$\Delta k_{par} = -\frac{dk_s}{d\omega_s} \Delta\omega + \frac{dk_i}{d\omega_i} \cos \Omega \Delta\omega - k_i \sin \Omega \frac{d\Omega}{d\omega_i} \Delta\omega = 0 \quad \times \cos(\Omega)$$

$$\Delta k_{perp} = \frac{dk_i}{d\omega_i} \sin \Omega \Delta\omega + k_i \cos \Omega \frac{d\Omega}{d\omega_i} \Delta\omega = 0 \quad \times \sin(\Omega)$$

## And addition

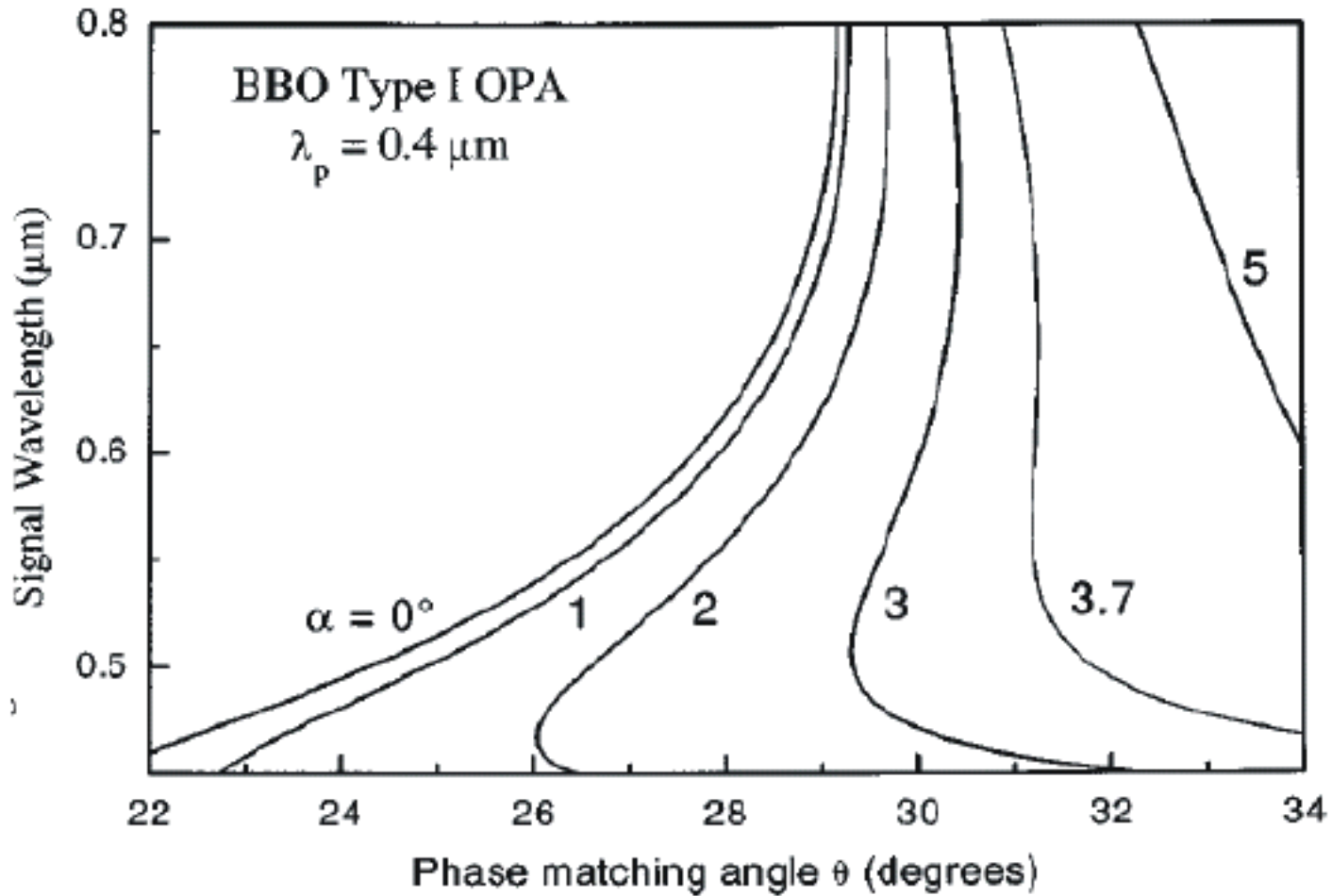
$$\frac{dk_i}{d\omega_i} - \cos \Omega \frac{dk_s}{d\omega_s} = 0$$

Correct  
index

$$v_{gs} - v_{gi} \cos \Omega = 0$$

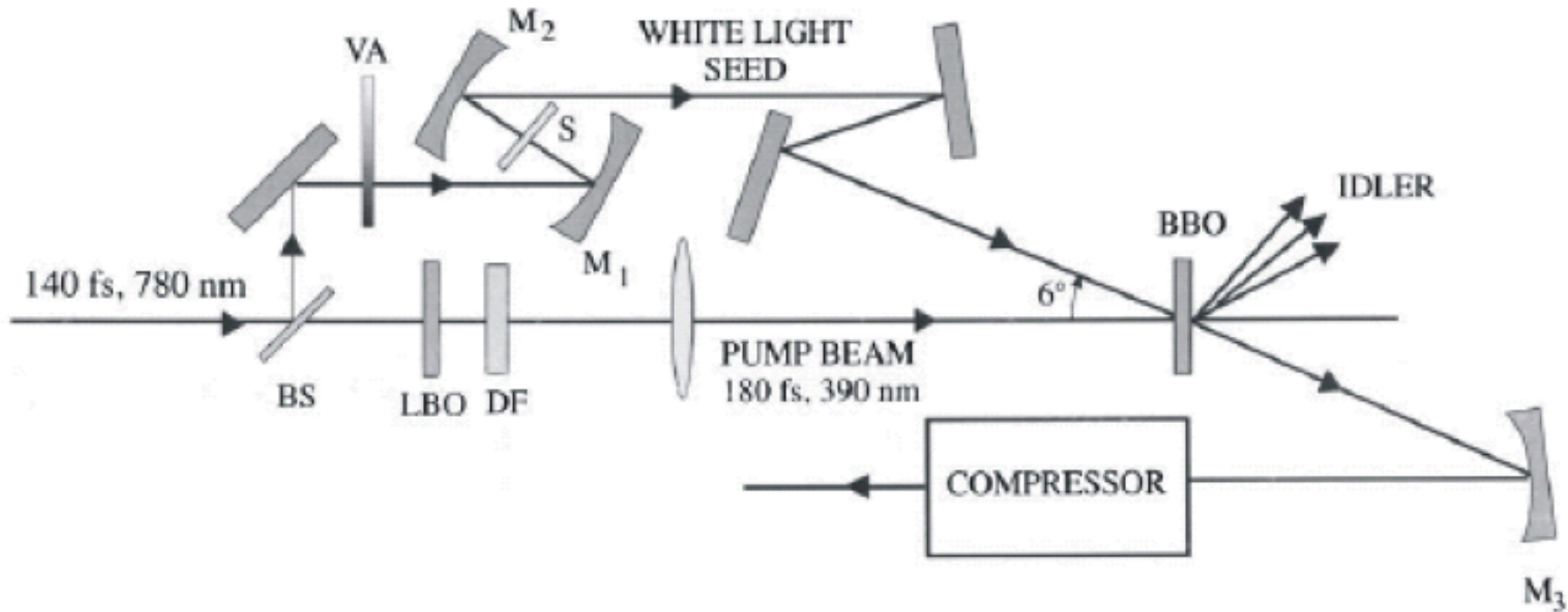
Only possible if:  $v_{gi} > v_{gs}$

$$\alpha = \arcsin \left[ \frac{1 - \frac{v_s^2}{v_i^2}}{1 + 2v_s n_s \lambda_i / v_i n_i \lambda_s + (n_s \lambda_i / n_i \lambda_s)^2} \right]$$



**Figure 12.40:** Phase-matching curves for a noncollinear type I BBO OPA pumped at  $\lambda_p = 0.4 \mu\text{m}$ , as a function of the pump-signal angle  $\alpha$ . [5]

# NOPA Layout

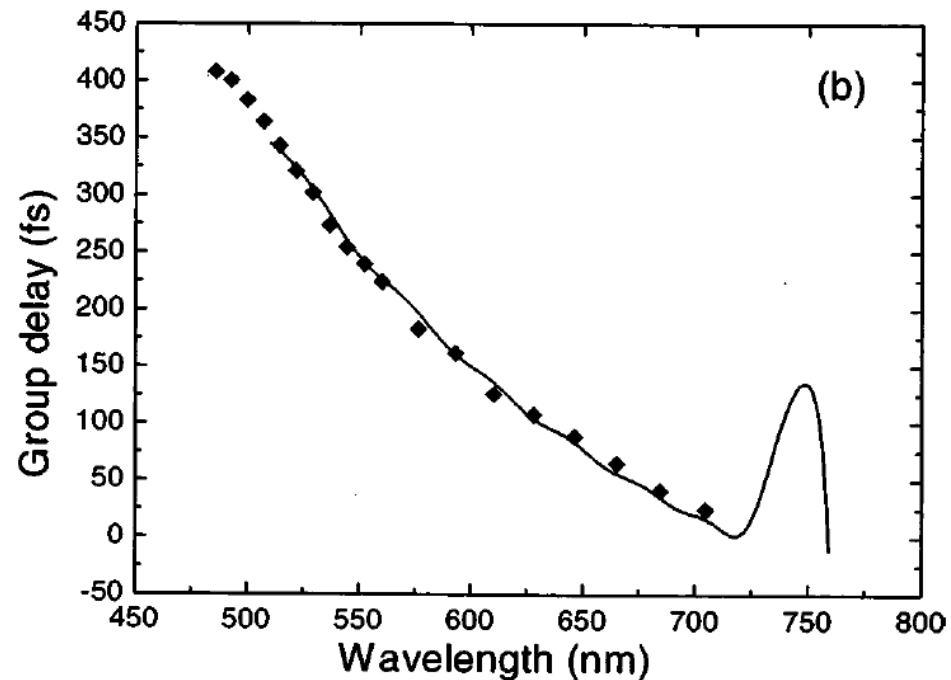
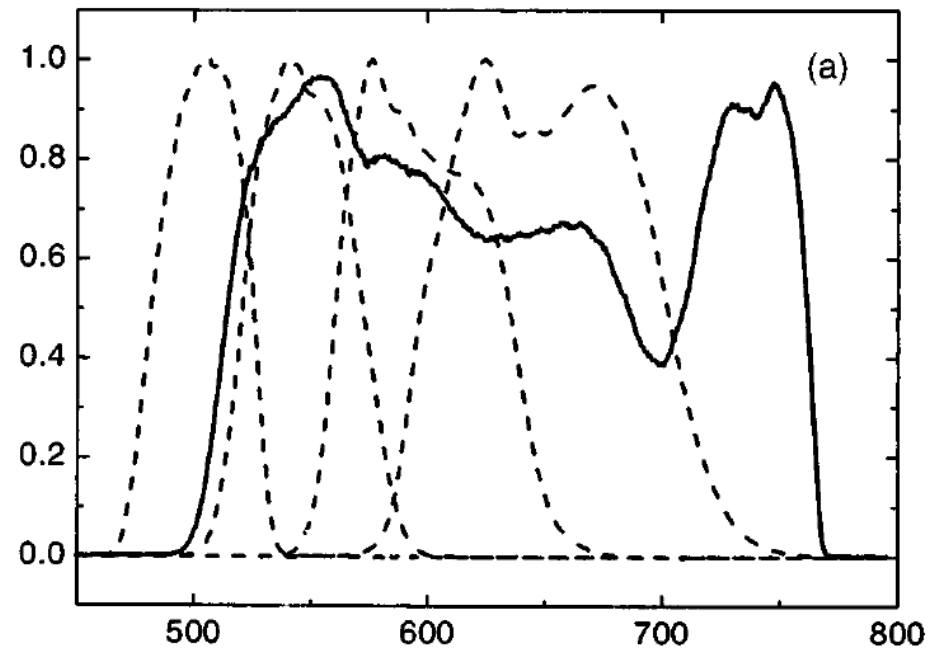


**Figure 12.41:** Scheme of a noncollinear visible OPA. BS: beam splitter; VA: variable attenuator; S: 1-mm-thick sapphire plate; DF: dichroic filter; M1, M2, M3, spherical mirrors.[5]

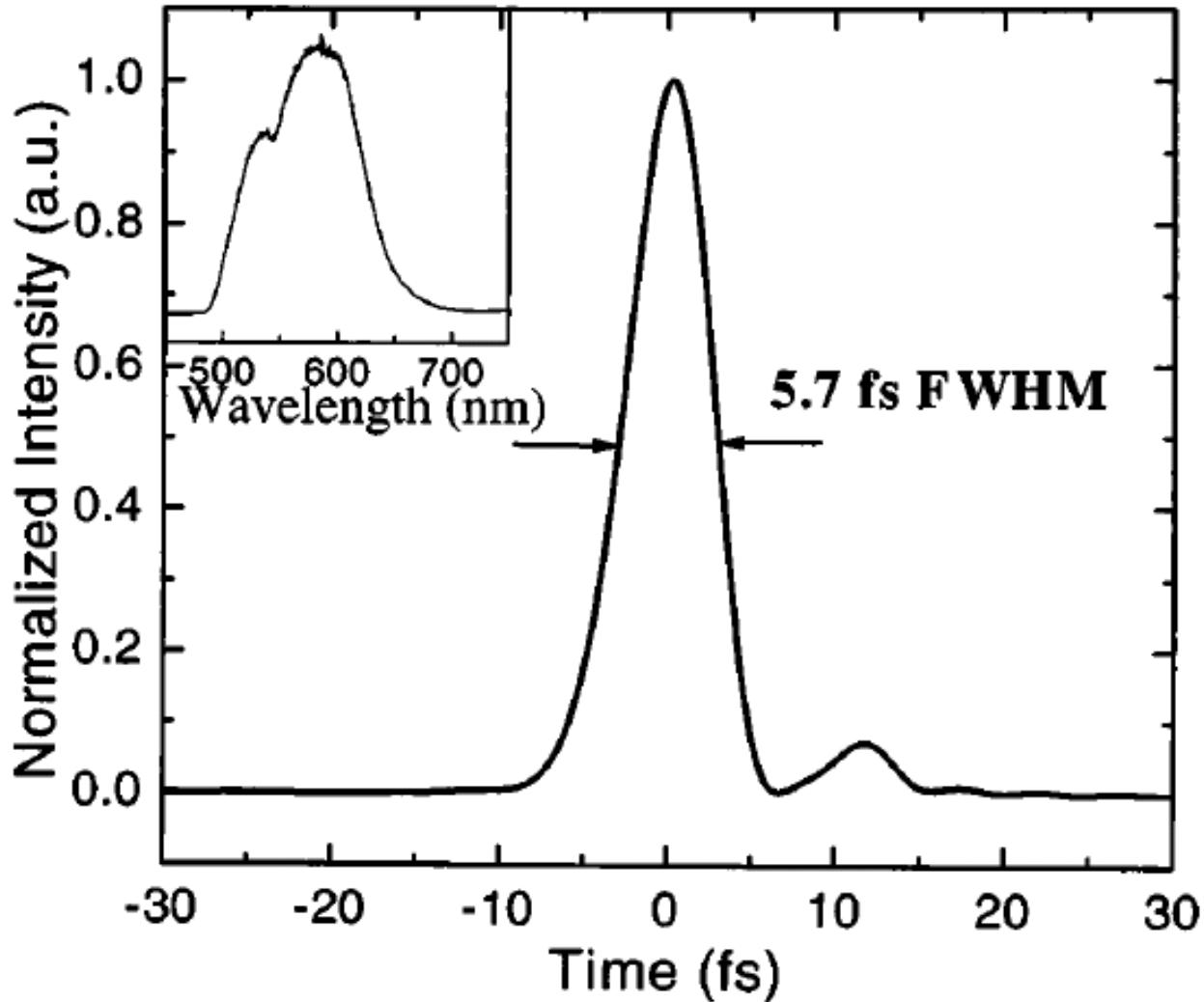
**Figure 12.42:**

a) Solid line: NOPA spectrum under optimum alignment conditions; dashed line: sequence of spectra obtained by increasing the white light chirp;

b) points: measured GD of the NOPA pulses; dashed line: GD after ten bounces on the ultrabroadband chirped mirrors.



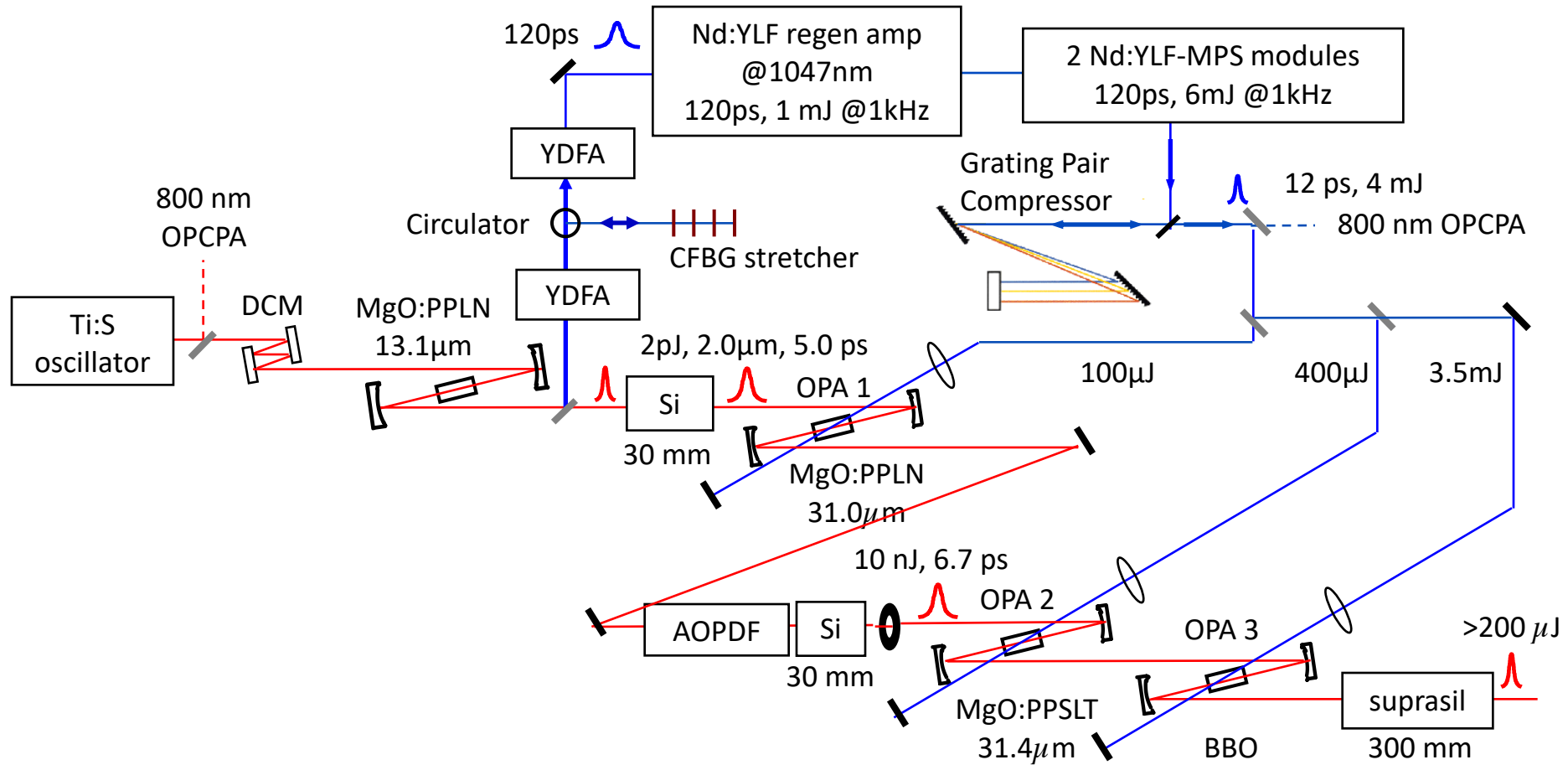




**Figure 12.43:** Reconstructed temporal intensity of the compressed NOPA pulse measured by the SPIDER technique. The inset shows the corresponding pulse spectrum.[5]

# Optical Parametric Chirped Pulse Amplifier (OPCPA)

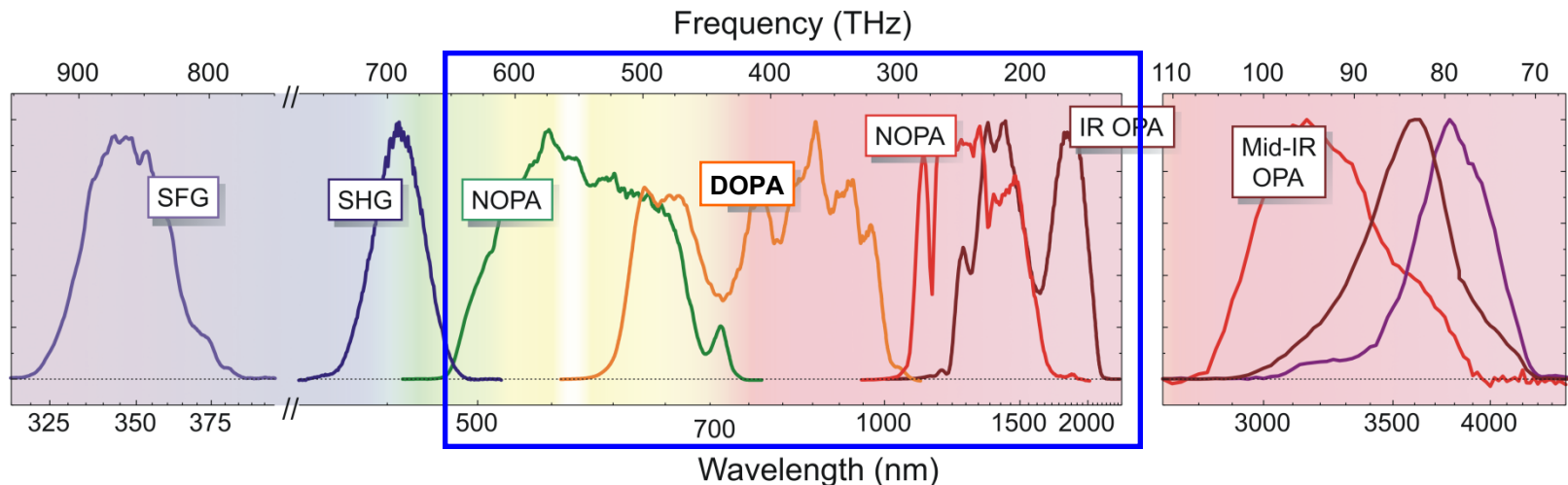
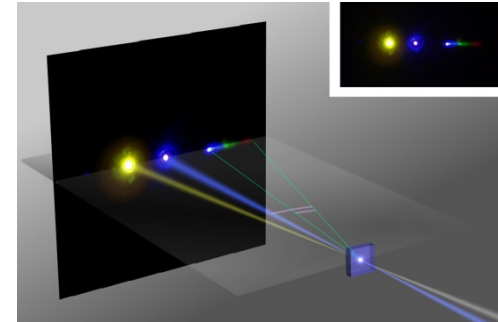
## 2- $\mu\text{m}$ OPCPA



# Optical Synthesis from OPAs

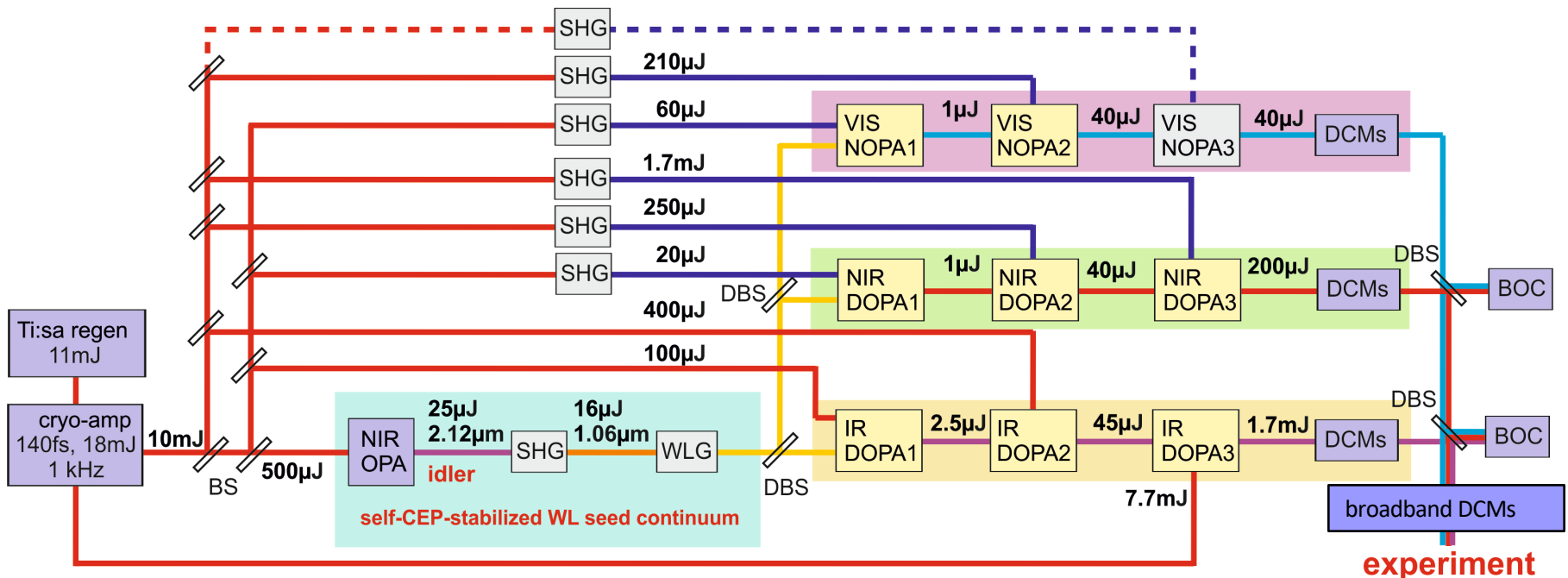
Combination of light from broadband Optical Parametric Amplifiers.

$\chi^{(2)}$  optical process in nonlinear crystals  
Broadband phase-matching

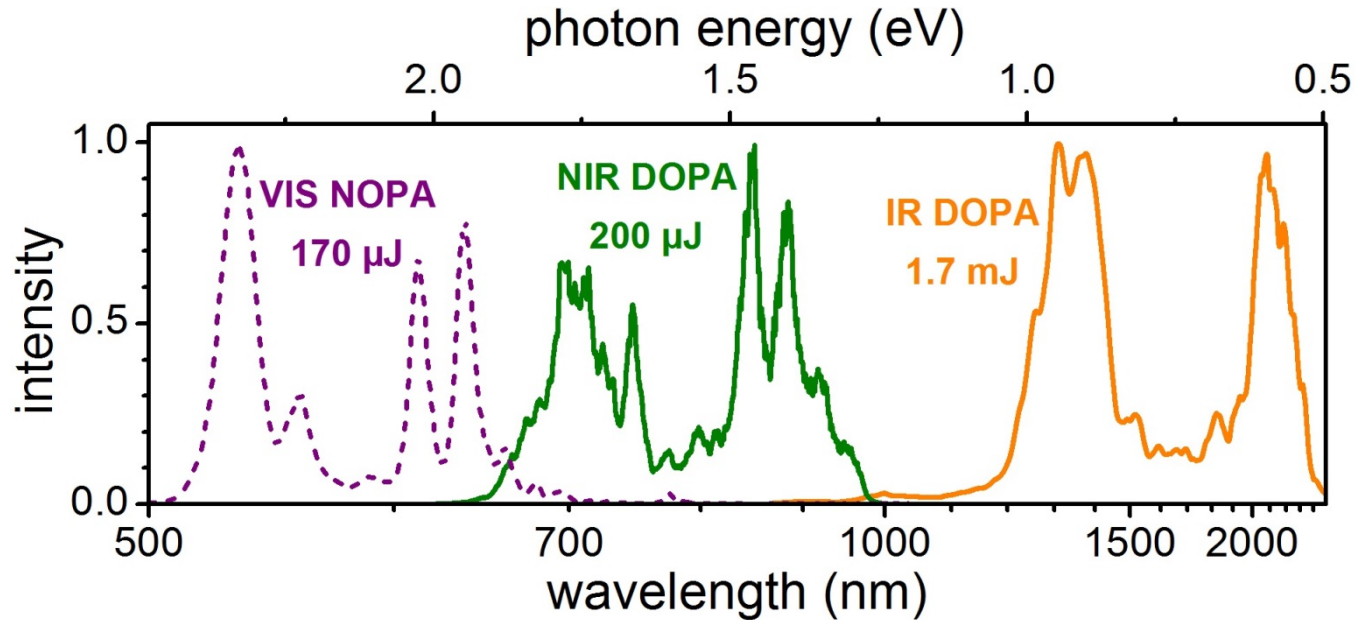


# Multi-millijoule Pulse Synthesis with OPAs

- **Two-octave-wide** waveform synthesis from OPAs at the **multi-mJ energy level**
- **passively CEP-stable** WLG seed [G. Cerullo *et al.*, Laser Photonics Rev. **5**, 323 (2010)]
- WLG seed split into 3 wavelength channels and amplified in 3 OPA stages each
- Three channels are individually compressed and coherently recombined
- relative timing is tightly locked using balanced optical cross-correlators (BOCs)



# Optical Pulse Synthesizer



VIS NOPA	NIR DOPA	IR DOPA
0.17 mJ signal	0.20-0.25 mJ signal	1.7 mJ octave-spanning signal
20% (0.8 mJ pump) pump-signal conversion efficiency	12-15% (1.7 mJ pump) pump-signal conversion efficiency	22% (7.7 mJ pump) pump-signal conversion efficiency
TL 5.6 fs	TL 5.2 fs	TL 5.2 fs
2.9 optical cycles @ $\lambda_c=573\text{nm}$	2.1 optical cycles @ $\lambda_c=750\text{nm}$	1.1 optical cycle @ $\lambda_c=1.4\mu\text{m}$