## Nonlinear Optics (WiSe 2018/19) Lecture 8: December 7, 2018

### **9** Optical Parametric Amplifiers and Oscillators

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[5] Largely follows the review paper by G. Cerullo *et al.*, "Ultrafast Optical Parametric Amplifiers," Rev. Sci. Instrum. 74, 1-17 (2003)

# 9 Optical Parametric Amplifiers and Oscillators 9.1 Optical Parametric Generation (OPG)



### **Optical Parametric Oscillator (OPO)**



#### double resonant: signal and idler resonant

#### single resonant: only signal resonant

Advantage: Widely tunable, both signal and idler can be used! For OPO to operate, less gain is necessary in contrast to an OPA

### **Nonlinear Optical Susceptibilities**

Total field: pump, signal and idler:

$$\vec{E}(\vec{r},t) = \sum_{\omega_a > 0} \sum_{i=1}^{3} \frac{1}{2} \left\{ \hat{E}_i(\omega_a) e^{j(\omega_a t - \vec{k}_a \vec{r})} + c.c. \right\} \vec{e_i}.$$

**Drives polarization in medium:** 

$$\vec{P}(\vec{r},t) = \sum_{n} \vec{P}^{(n)}(\vec{r},t)$$

Polarization can be expanded in power series of the electric field:

$$\vec{P}^{(n)}(\vec{r},t) = \sum_{\omega_b > 0} \sum_{i=1}^3 \frac{1}{2} \left\{ P_i^{(n)}(\omega_b) e^{j(\omega_b t - \vec{k}_b' \vec{r})} + c.c. \right\} \vec{e}_i.$$

**Defines susceptibility tensor:** 

$$P_i^{(n)}(\omega_b) = \frac{\varepsilon_0}{2^{m-1}} \sum_P \sum_{j\dots k} \chi_{ij\dots k}^{(n)}(\omega_b : \omega_1, \dots, \omega_n) E_j(\omega_1) \cdots E_k(\omega_n)$$
$$\omega_b = \sum_{i=1}^n \omega_i \text{ and } \mathbf{k}'_b = \sum_{i=1}^n \mathbf{k}_i$$

### **Special Cases**

$$\hat{P}_i^{(2)}(\omega_3) = \varepsilon_0 \sum_{jk} \chi_{ijk}^{(2)}(\omega_3 : \omega_1, -\omega_2) \hat{E}_j(\omega_1) \hat{E}_k^*(\omega_2),$$
  
$$\omega_3 = \omega_1 - \omega_2 \text{ und } \mathbf{k}_3' = \mathbf{k}_1 - \mathbf{k}_2.$$

 $(\longrightarrow \text{Difference Frequency Generation (DFG)})$ 

$$\hat{P}_i^{(2)}(\omega_2) = \varepsilon_0 \sum_{jk} \chi_{ijk}^{(2)}(\omega_2 : \omega_3, -\omega_1) \hat{E}_j(\omega_3) \hat{E}_k^*(\omega_1),$$
$$\omega_2 = \omega_3 - \omega_1 \text{ und } \mathbf{k}_2' = \mathbf{k}_3 - \mathbf{k}_1.$$

 $(\longrightarrow \text{Parametric Generation (OPG)})$ 

$$\hat{P}_i^{(3)}(\omega_4) = \frac{6\varepsilon_0}{4} \sum_{jkl} \chi_{ijkl}^{(3)}(\omega_4 : \omega_1, \omega_2, -\omega_3) \hat{E}_j(\omega_1) \hat{E}_k(\omega_2) \hat{E}_l^*(\omega_3)$$
  
$$\omega_4 = \omega_1 + \omega_2 - \omega_3 \text{ und } \mathbf{k}_4' = \mathbf{k}_1 + \mathbf{k}_2 - \mathbf{k}_3.$$

 $(\longrightarrow$  Four Wave Mixing (FWM))

## 9.2 Continuous-wave OPA

Wave equation :

$$\left(\Delta - \frac{1}{c_0^2} \frac{\partial^2}{\partial t^2}\right) \vec{E} = \mu_0 \frac{\partial^2}{\partial t^2} \vec{P}.$$

Include linear and second-order terms:

$$\left(\Delta - \frac{1}{c_0^2} \frac{\partial^2}{\partial t^2}\right) \vec{E} = \mu_0 \frac{\partial^2}{\partial t^2} \left(\vec{P}^{(l)}(\vec{r}, t) + \vec{P}^{(2)}(\vec{r}, t)\right)$$

Changes group and phase velocities of waves

 $k(\omega)$ 

Nonlinear interaction of waves

z-propagation only:

$$\vec{E}_{p,s,i}(z,t) = \operatorname{Re}\left\{E_{p,s,i}(z) \ e^{j(\omega_{p,s,i}t-k_{p,s,i}\ z)}\vec{e}_{p,s,i}\right\}$$
Wave amplitudes

$$\vec{P}_{p,s,i}^{(2)}(z,t) = \operatorname{Re}\left\{P_{p,s,i}^{(2)}(z) \ e^{j\left(\omega_{p,s,i}t - k'_{p,s,i}z\right)}\vec{e}_{p,s,i}\right\}$$

Separate into three equations for each frequency component: Slowly varying amplitude approximation:

$$\begin{aligned} d_{p,s,i}^2 E(z) \ /dz^2 << \ 2k \ dE_{p,s,i}(z) \ /dz, \\ \frac{\partial E_{p,s,i}(z)}{\partial z} = -\frac{jc_0^2 \omega_{p,s,i}}{2n(\omega_{p,s,i})} P_{p,s,i}^{(2)}(z) \ e^{-j \binom{k'_{p,s,i} - k_{p,s,i}}{2n(\omega_{p,s,i})} z} \end{aligned}$$

Introduce phase mismatch:  $\Delta k = k(\omega_p) - k(\omega_s) - k(\omega_i)$ 

and effective nonlinearity and coupling coefficients:

$$d_{eff} = \frac{1}{2} \chi_{ijk}^{(2)}(\omega_p : \omega_s, \omega_i), \quad \kappa_{p,s,i} = \omega_{p,s,i} \ d_{eff} / (n_{p,s,i}c_0)$$

#### **Coupled wave equations:**

$$\begin{aligned} \frac{\partial E_p(z)}{\partial z} &= -j\kappa_p \ E_s(z)E_i(z) \ e^{j\Delta kz} \ ,\\ \frac{\partial E_s(z)}{\partial z} &= -j\kappa_s \ E_p(z)E_i^*(z) \ e^{-j\Delta kz}, \qquad \mathbf{X} \ n_{p,s,i}c_0\varepsilon_0 E_{p,s,i}^*/2\\ \frac{\partial E_i(z)}{\partial z} &= -j\kappa_i \ E_p(z)E_s^*(z) \ e^{-j\Delta kz}. \end{aligned}$$

$$I_{p,s,i} = \frac{n_{p,s,i}}{2Z_{F_0}} |E_{p,s,i}|^2$$

**Manley-Rowe relations:** 

$$-\frac{1}{\omega_p}\frac{dI_p}{dz} = \frac{1}{\omega_s}\frac{dI_s}{dz} = \frac{1}{\omega_i}\frac{dI_i}{dz}$$

- -

### **9.4 Theory of Optical Parametric Amplification**

Undepleted pump approximation:  $E_p = const.$ 

$$\frac{\partial E_s(z)}{\partial z} = -j\kappa_s E_p E_i^*(z) e^{-j\Delta kz},$$
$$\frac{\partial E_i(z)}{\partial z} = -j\kappa_i E_p E_s^*(z) e^{-j\Delta kz}.$$

with:

$$E_s(z = 0) = E_s(0)$$
  $E_i(z = 0) = 0$ 

 $E_s(z) \ E_s(0) \ e^{gz-j\Delta kz/2}$  and  $E_i(z) \ E_i(0) \ e^{gz-j\Delta kz/2}$ 

$$\left|\begin{array}{c}g-j\frac{\Delta k}{2} & j\kappa_s \ E_p\\ j\kappa_i \ E_p^* & g+j\frac{\Delta k}{2}\end{array}\right| = 0$$

$$g = \sqrt{\Gamma^2 - \left(\frac{\Delta k}{2}\right)^2}, \text{ with } \Gamma = \sqrt{\kappa_i \ \kappa_s \ |E_p|^2}.$$

gain

max. gain, when phase matched

#### Maximum gain

$$\Gamma^2 = \frac{\omega_s \omega_i}{n_s n_i c_0^2} d_{eff}^2 |E_p|^2 = \frac{2Z_{F_0} \omega_s \omega_i}{n_p n_s n_i c_0^2} d_{eff}^2 I_p \qquad FOM = \frac{d_{eff}}{\sqrt{\lambda_s \lambda_i n_p n_s n_i}}$$

#### **General solutions:**

$$E_s(z) = \{E_s(0) \cosh gz + B \sinh gz\} e^{-j\Delta kz/2}$$

$$B = -j\frac{\Delta k}{2g}E_s(0) - j\frac{\kappa_1}{g}E_pE_i^*(0)$$

 $E_{i}(z)=\left\{ E_{i}\left(0\right)\cosh gz+D\sinh gz\right\} e^{-j\Delta kz/2}$ 

$$D = -j\frac{\Delta k}{2g}E_i\left(0\right) - j\frac{\kappa_2}{g}E_p^*E_s^*\left(0\right)$$

Here:

$$I_s(L) = I_s(0) \left[ 1 + \frac{\Gamma^2}{g^2} \sinh^2 gL \right]$$
$$I_i(L) = I_s(0) \frac{\omega_i}{\omega_s} \frac{\Gamma^2}{g^2} \sinh^2 gL.$$

For large gain:  $\Gamma L >> 1$ 

$$\begin{split} I_s(L) &= \frac{1}{4} I_s(0) \ e^{2\Gamma L}, \\ I_i(L) &= \frac{1}{4} I_s(0) \ \frac{\omega_i}{\omega_s} \ e^{2\Gamma L} \end{split} \longrightarrow G = \frac{I_s(L)}{I_s(0)} = \frac{1}{4} \ e^{2\Gamma L} \end{split}$$

#### **Figure of merit:**

$$FOM = \frac{d_{eff}}{\sqrt{\lambda_s \lambda_i n_p n_s n_i}}$$





**Fig. 9.3** Parametric gain for an OPA at the pump wavelength  $\lambda_p = 0.8 \ \mu m$  and the signal wavelength  $\lambda_s = 1.2 \ \mu m$ , using type-I phase matching in BBO ( $d_{eff} = 2 \ pm/V$ ).



**Fig. 9.4** Parametric gain for an OPA at the pump wavelength  $\lambda_p = 0.4 \ \mu m$  and the signal wavelength  $\lambda_s = 0.6 \ \mu m$ , using type-I phase matching in BBO ( $d_{eff} = 2 \ pm/V$ ).

## 9.4 Phase Matching



Uniaxial crystal: n<sub>e</sub> < n<sub>o</sub>

#### **Type I: noncritical**

**Type I: critical** 

λp



Fig. 9.5 Type-I noncritical phase matching.

Fig. 9.6 Type-I critical phase matching by adjusting the angle  $\theta$  between wave vector of the propagating beam and the optical axis.

λ

no

n<sub>e</sub>

λ

Wavelength

## **9.4 Phase Matching**



#### **Critical Phase Matching**

$$\begin{aligned} n_{ep}(\theta)\omega_p &= n_{os}\omega_s + n_{oi}\omega_i \\ \frac{1}{n_{ep}(\theta)^2} &= \frac{\sin^2\theta}{n_{ep}^2} + \frac{\cos^2\theta}{n_{op}^2} \\ \theta &= \arcsin\left[\frac{n_{ep}}{n_{ep}(\theta)}\sqrt{\frac{n_{op}^2 - n_{ep}^2(\theta)}{n_{op}^2 - n_{ep}^2}}\right] \end{aligned}$$

#### 9.4 Phase Matching



**Fig. 9.7** Angle tuning curves for a BBO OPA at the pump wavelength  $\lambda_p$ =0.8 µm for type-I phase matching (dotted line), type-II ( $o_s + e_i \rightarrow e_p$ ) phase matching (solid line), and type-II ( $e_s + o_i \rightarrow e_p$ ) phase matching (dashed line).



**Fig. 9.8** Angle tuning curves for a BBO OPA at the pump wavelength  $\lambda_p=0.4 \mu m$  for type-I phase matching (dotted line), type-II ( $o_s + e_i \rightarrow e_p$ ) phase matching (solid line), and type-II ( $e_s + o_i \rightarrow e_p$ ) phase matching (dashed line).

## 9.5 Quasi Phase Matching



## Periodically poled crystal

**Fig.12.30:** Variation of  $d_{eff}$  in a quasi phase matched material as a function of propagation distance.

$$d_{eff}(z) = \sum_{m=-\infty}^{+\infty} d_m e^{jm\kappa z}$$
$$\frac{\partial E_p(z)}{\partial z} = -j\kappa_p \ E_s(z)E_i(z) \ e^{j\Delta kz}$$

### 9.6 Ultrashort-Pulse Optical Parametric Amplification

$$\vec{E}_{p,s,i}(z,t) = \operatorname{Re}\left\{E_{p,s,i}(z,t) \ e^{j(\omega_{p,s,i}t-k_{p,s,i}\ z)}\vec{e}_{p,s,i}\right\}$$
nvelopes

Pulse envelopes

$$\begin{aligned} \frac{\partial E_p}{\partial z} + \frac{1}{v_p} \frac{\partial E_p}{\partial t} &= -j\kappa_p \ E_s E_i \ e^{j\Delta kz} \ ,\\ \frac{\partial E_s}{\partial z} + \frac{1}{v_s} \frac{\partial E_s}{\partial t} &= -j\kappa_s \ E_p E_i^* \ e^{-j\Delta kz} ,\\ \frac{\partial E_i}{\partial z} + \frac{1}{v_i} \frac{\partial E_s}{\partial t} &= -j\kappa_i \ E_p E_s^* \ e^{-j\Delta kz} ,\end{aligned}$$

 $v_{p,s,i} = \left. dk/d\omega \right|_{\omega_{p,s,i}}$  are the corresponding group velocities

$$\begin{aligned} t' &= t - z/v_p & \frac{\partial E_p}{\partial z} &= -j\kappa_p \ E_s E_i \ e^{j\Delta kz} \ ,\\ \frac{\partial E_s}{\partial z} &+ \left(\frac{1}{v_s} - \frac{1}{v_p}\right) \frac{\partial E_s}{\partial t} &= -j\kappa_s \ E_p E_i^* \ e^{-j\Delta kz},\\ \frac{\partial E_i}{\partial z} &+ \left(\frac{1}{v_i} - \frac{1}{v_p}\right) \frac{\partial E_s}{\partial t} &= -j\kappa_i \ E_p E_s^* \ e^{-j\Delta kz}. \end{aligned}$$

#### **Temporal walkoff Group Velocity Mismatch (GVM)**

Group velocity mismatch 8 (fs/mm)

Pump pulse width  $\ell_{jp} = \frac{\tau}{\delta_{jp}}, \text{ with } \delta_{jp} = \left(\frac{1}{v_j} - \frac{1}{v_p}\right)$ j=s,i50 Type II( $o_s + e_{i} - e_{p}$ )  $\delta_{ip}$ Type I,  $\delta_1$ 0 -50 Type II( $o_s + e_i \rightarrow e_p$ )  $\delta_{sp}$ -100 Type Ι, δ<sub>ip</sub> BBO OPA  $\lambda_p = 0.8 \ \mu m$ -150 1.2 1.3 1.5 1.0 1.1 1.4 1.6 OPA signal wavelength (µm)

**Fig. 9.9:** Pump-signal ( $\delta_{sp}$ ) and pump-idler ( $\delta_{ip}$ ) group velocity mismatch curves for a BBO OPA at the pump wavelength  $\lambda_{\rm p}$ =0.8  $\mu m$  for type-I phase matching (solid line) and type-II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line).



**Fig. 9.10:** Pump-signal ( $\delta_{sp}$ ) and pump-idler ( $\delta_{ip}$ ) group velocity mismatch curves for a BBO OPA at the pump wavelength  $\lambda_p=0.4 \ \mu m$  for type-I phase matching (solid line) and type-II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line).



**Fig. 9.11:** Signal pulse evolution for a BBO type-I OPA with  $\lambda_p = 0.4 \mu m$ ,  $\lambda_s = 0.7 \mu m$ , for different lengths L of the nonlinear crystal. Pump intensity is 20 GW/cm<sup>2</sup>. Time is normalized to the pump pulse duration and the crystal length to the pump-signal pulse splitting length. [5]



Figure 9.12: Signal pulse evolution for a BBO type-I OPA with  $\lambda_p = 0.8 \ \mu m$ ,  $\lambda_s = 1.5 \ \mu m$ , for different lengths L of the nonlinear crystal. Pump intensity is 20 GW/cm<sup>2</sup>. Time is normalized to the pump pulse duration and the crystal length to the pump-signal pulse splitting length. [5]

## **OPA Bandwidth**

$$\Delta \omega_s \longrightarrow \omega_s + \Delta \omega \qquad \omega_i \longrightarrow \omega_i - \Delta \omega$$
$$\Delta k = -\frac{dk_s}{d\omega} \Delta \omega + \frac{dk_i}{d\omega} \Delta \omega = \left(\frac{1}{v_i} - \frac{1}{v_s}\right) \Delta \omega$$

**Bandwidth limitation due to GVM** 

$$\Delta f = -\frac{2\sqrt{\ln 2}}{\pi} \sqrt{\frac{\Gamma}{L}} \frac{1}{\left|\frac{1}{v_i} - \frac{1}{v_s}\right|}$$

For signal-idler group velocity matching:

$$\Delta f = -\frac{2\sqrt[4]{\ln 2}}{\pi} \sqrt[4]{\frac{\Gamma}{L}} \frac{1}{\left|\frac{d^2k_s}{d\omega^2} + \frac{d^2k_s}{d\omega^2}\right|}.$$



**Fig. 9.13:** Phase matching bandwidth for a BBO OPA at the pump wavelength  $\lambda_p=0.8 \ \mu m$  for type-I phase matching (solid line) and type-II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line). Crystal length is 4 mm and pump intensity 50 GW/cm<sup>2</sup>.



**Fig. 9.14:** Phase matching bandwidth for a BBO OPA at the pump wavelength  $\lambda_p=0.4 \mu m$  for type-I phase matching (solid line) and type-II ( $o_s + e_i \rightarrow e_p$ ) phase matching (dashed line). Crystal length is 2 mm and pump intensity 100 GW/cm<sup>2</sup>.

## **9.7 Optical Parametric Amplifier Designs**



**Fig. 9.15:** Scheme of an ultrafast optical parametric amplifier. SEED: seed generation stage; DL1, DL2: delay lines; OPA1, OPA2 parametric amplification stages; COMP: compressor.

### **Near-IR OPA**



**Fig. 9.16:** Scheme of a near-IR OPA. DL: delay lines; WL: white light generation stage; DF: dichroic filter. [5]

## 9.8 Noncollinear Optical Parametric Amplifier (NOPA)



**Fig. 9.17:** a) Schematic of a noncollinear interaction geometry; b) representation of signal and idler pulses in the case of collinear interaction; and c) same as b) for noncollinear interaction.

#### Phase-matching condition: vector condition:

$$\Delta k_{par} = k_p \cos \alpha - k_s - k_i \cos \Omega = 0$$
  
$$\Delta k_{perp} = k_p \sin \alpha - k_i \sin \Omega = 0$$

#### Variation on phase matching condition by $\Delta \omega$

$$\begin{split} \Delta k_{par} &= -\frac{dk_s}{d\omega_s} \Delta \omega + \frac{dk_i}{d\omega_i} \cos \Omega \ \Delta \omega - k_i \sin \Omega \frac{d\Omega}{d\omega_i} \Delta \omega = 0 \quad \mathbf{X} \quad \cos(\Omega) \\ \Delta k_{perp} &= \frac{dk_i}{d\omega_i} \sin \Omega \ \Delta \omega + k_i \cos \Omega \frac{d\Omega}{d\omega_i} \Delta \omega = 0 \quad \mathbf{X} \quad \sin(\Omega) \end{split}$$

#### and addition

$$\frac{dk_i}{d\omega_i} - \cos\Omega \frac{dk_s}{d\omega_s} = 0$$
Correct
$$v_{gs} - v_{gi} \ \cos\Omega = 0$$
index

Only possible if:  $v_{gi}$ 

$$v_{gi} > v_{gs}$$

$$\alpha = \arcsin\left[\frac{1 - \frac{v_s^2}{v_i^2}}{1 + 2v_s n_s \lambda_i / v_i n_i \lambda_s + (n_s \lambda_i / n_i \lambda_s)^2}\right]$$



**Fig. 9.18:** Phase-matching curves for a noncollinear type-I BBO OPA pumped at  $\lambda_p$ =0.4  $\mu$ m, as function of the pump-signal angle  $\alpha$ . [5]



**Fig. 9.19:** Scheme of a noncollinear visible OPA. BS: beam splitter; VA: variable attenuator; S: 1-mm-thick sapphire plate; DF: dichroic filter; M1 ,M2 , M3 , spherical mirrors. [5]

Fig. 9.20: a) Solid line: NOPA spectrum under optimum alignment conditions; dashed line: sequence of spectra obtained by increasing the white light chirp; b) points: measured group delay (GD) of the NOPA pulses; dashed line: GD after ten bounces on the ultrabroadband chirped mirrors.





**Fig. 9.21:** Reconstructed temporal intensity of the compressed NOPA pulse measured by the SPIDER technique. The inset shows the corresponding pulse spectrum. [5]

## 9.9 Optical Parametric Chirped-Pulse Amplifier (OPCPA)

2-μm OPCPA

